

Supporting Information:

Greenhouse Gas Footprint, Water-Intensity, and, Production Cost of Bio-Based Isopentenol as a Renewable Transportation Fuel

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S1. Data sources

S1.1. Input parameters and required material and energy for feedstock supply system

Table S1. Major input parameters used in the feedstock supply model

Parameter	Unit	μ	a	b	σ	Probability distribution
Required dry biomass (assumed)	t/day	2,000.0	-	-	-	None
Biorefinery working days (assumed)	days/yr	330.0	-	-	-	None
Moisture content ¹⁻³	%	59.7	40.0	70.0	10.7	Triangular
Safety stock ⁴	%	12.5	8.0	25.0	8.8	Triangular
Dry matter loss (supply chain) ^{4,5}	%	11.6	4.2	25.0	6.6	Lognormal
Dry matter loss (forage harvester) ^{6,7}	%	2.4	0.8	4.0	-	Triangular
Harvest window ⁸	days/yr	31.5	15.0	75.0	14.6	Triangular
Harvesting hours ^{λ}	h/day	16.0	8.0	24.0	8.0	Triangular
Land utilization for sorghum farming ^{ω}	%	5.0	2.0	10.0	-	Triangular
Road winding factor ⁹⁻¹²	-	1.5	1.1	3.5	0.4	Normal
Nitrogen ^{3,13-16}	kg/ha	121.24	48.0	217.0	51.88	Triangular
Phosphorus ^{3,13,15}	kg/ha	23.89	9.30	67.25	16.74	Triangular
Potassium ^{3,13,15}	kg/ha	168.09	20.00	293.66	-	Triangular
Price of nitrogen ¹⁷⁻²¹	\$/kg	1.06	0.60	1.40	0.34	Triangular
Price of phosphorus ¹⁷⁻²¹	\$/kg	1.01	0.82	1.20	0.15	Triangular
Price of potassium ¹⁷⁻²¹	\$/kg	1.09	0.91	1.26	0.14	Triangular
Herbicides ²²⁻²⁴	kg/ha	3.13	1.79	5.60	-	Triangular
Herbicides ²²⁻²⁵	\$/ha	62.12	24.46	111.2	-	Triangular

^{λ} Assumed based on the current harvesting practices of biomass sorghum.

^{ω} Percentage of the total area (including land, water bodies, and others) around the biorefinery.

Note: μ = average value; a = minimum value; b = maximum value; σ = standard deviation

Selection of probability distribution: The probability distribution is selected based on the data gathered from several sources or historical data. In the case of the limited data sources, either triangular or uniform probability distribution is selected. The uniform probability distribution is chosen if the input parameter is dependent on the types of process technology or operating conditions.

Table S2. Material and energy data generated from the feedstock supply model²⁶

Lifecycle stage	Materials	Units	μ	a	b	σ
Nutrient	N	kg/t-DBS	7.35	2.03	22.39	4.18
	P	kg/t-DBS	1.45	0.12	9.92	1.54
	K	kg/t-DBS	10.19	0.99	54.62	7.28
Chopping	Diesel	L/t-DBS	3.09	1.10	9.36	1.29
Infield transportation	Diesel	L/t-DBS	0.38	0.21	0.77	0.09
Biorefinery transport	Diesel	L/t-DBS	3.18	0.99	9.61	1.32
Storage at depot	Tarp	m ² /t-DBS	4.30	2.78	8.26	0.79
	Gravel	m ² /t-DBS	3.51	2.27	6.74	0.65

Note: μ : baseline (average) value; a: minimum value; b: maximum value; and σ : standard deviation. DBS refers to the dry biomass sorghum delivered to the biorefinery

S1.2. Major operating and process parameters used to develop the downstream process model

Table S3. Modeling inputs and their probability distributions

Parameters	Units	μ	a	b	σ	Probability distribution
Cost of sorghum biomass ²⁶	\$/t-dry	101.8	60.00	137	4.82	Lognormal
Sorghum biomass composition²⁷⁻³⁴						
Acetate	wt%	2.20	0.90	2.90		Constant
Ash	wt%	7.70	2.20	10.94	3.49	Lognormal
Cellulose	wt%	35.80	20.50	44.02	5.31	Lognormal
Hemicellulose	wt%	22.92	14.50	29.79	3.80	Lognormal
Lignin	wt%	16.52	9.89	20.29	2.70	Lognormal
Proteins	wt%	4.39	3.88	5.16	0.68	Constant
Ionic liquid (IL) Pretreatment						
Solid loading rate ³⁵⁻³⁷	wt%	30.00	20.00	40.00		Triangular
IL loading rate ³⁶	kg/kg-biomass	0.29	0.25	0.35		Triangular
IL-cost ^{36,38}	\$/kg	2.00	1.43	5.00		Triangular
Sulfuric acid loading ^{36,38}	kg-/kg-IL	0.16	0.15	0.17		Triangular
Sulfuric acid price ^{35,39,40}	\$/kg	0.14	0.03	0.28	0.11	Triangular
Lignin to soluble lignin ^{36,38}	wt%	65.00	60	70		Constant
Pretreatment time ^{36,38}	h	3.00	2.5	3.4		Triangular
Enzymatic hydrolysis³⁶⁻³⁸						
Enzyme loading rate	mg-protein/g-glucan	20.00	7	20		Uniform
Initial solid loading rate	wt%	20.00	20	30		Uniform
Cellulose to glucose	wt%	84.00	84	95		Uniform
Xylan to xylose	wt%	80.00	75	90		Uniform
Hydrolysis time	h	48.00	36	72		Triangular
Enzyme price	\$/kg-protein	5.00	4	6		Triangular
Bioconversion						
Aeration rate (aerobic) ⁴¹⁻⁴³	VVM	1.00	1.00	2.00		Triangular
Aeration rate (micro-aerobic) ^{43,44,44,45}	VVM	0.5	0.2	1.5		Triangular
Power consumption (aerobic) ⁴⁶	kW/m ³	3.00	2.00	5.00		Triangular
Power consumption (micro-aerobic) ⁴⁶	kW/m ³	0.35	0.2	0.6		Triangular
Power dissipation to heat (aerobic) ^{46,47}	%	80.00	70.00	100.00		Triangular
Power dissipation to heat (micro-aerobic) ^{46,47}	%	40.00	30.00	50.00		Triangular
Bioconversion time ⁴⁸⁻⁵⁰	h	72.00	48.00	84.00		Uniform
Glucose to isopentenol ⁴⁸⁻⁵⁰	wt%	20.45	14	40.9		Uniform
Xylose to isopentenol ⁴⁸⁻⁵⁰	wt%	20.45	14	40.9		Uniform
Corn steep liquor price ^{35,39,40}	\$/kg	0.06	0.05	0.07		Triangular
DAP price ^{35,39,40}	\$/kg	0.97	0.69	1.10		Triangular
Recovery and separation						
Recovery of isopentenol (assumed)	wt%	95	95	99		Uniform
IL-recovery ^{36,37,51}	wt%	97	85.00	99.0		Triangular
Wastewater treatment						
Organic matter to biogas conversion ³⁵	wt%	86.00	85	91		Triangular
Onsite energy generation						
Boiler chemicals price ³⁵	\$/kg	5.00	4.00	6.00		Triangular
Natural gas price ^b	\$/kg	0.22	0.10	0.44	0.10	Lognormal

Note: μ : baseline (average) value; a: minimum value; b: maximum value; and σ : standard deviation. Unless otherwise specified data summarized in this table were gathered from recent studies.³⁶⁻³⁸ The uncertainty analysis for each product yield scenario was run by fixing the product yield and considering variabilities present in other input parameters. The probability distribution is selected based on the data gathered from several sources or historical data. In the case of the limited data sources, either triangular or uniform probability distribution is selected. The uniform probability distribution is chosen if the input parameter is dependent on the types of process technology or operating conditions.

^b<https://www.eia.gov/dnav/ng/hist/rngwhhdA.htm>

S1.3. Material and energy data obtained from process model after 5000 trials

Table S4. Outputs from techno-economic model developed in SuperPro Designer

Lifecycle stage	Parameter	Unit	μ	a	b	σ
Feedstock supply (composition)	Acetate	kg/kg-isopentenol	0.21	0.07	0.37	0.04
	Ash	kg/kg-isopentenol	0.72	0.07	3.13	0.30
	Cellulose	kg/kg-isopentenol	3.36	1.35	5.84	0.67
	Extractive	kg/kg-isopentenol	0.98	0.00	4.98	0.67
	Hemicellulose	kg/kg-isopentenol	2.15	0.71	4.10	0.46
	Lignin	kg/kg-isopentenol	1.55	0.44	3.16	0.37
Feedstock handling	Moisture	kg/kg-isopentenol	1.04	0.38	1.85	0.22
	Electricity	kWh/kg-isopentenol	0.07	0.03	0.13	0.02
Pretreatment	Steam 226°C	kg/kg-isopentenol	0.74	0.20	1.43	0.17
	Electricity	kWh/kg-isopentenol	0.08	0.03	0.14	0.02
	Ionic liquid	kg/kg-isopentenol	0.10	0.0002	0.81	0.13
	Sulfuric Acid	kg/kg-isopentenol	0.73	0.25	1.49	0.17
	Water	kg/kg-isopentenol	12.11	4.72	21.98	2.57
Hydrolysis and Bioconversion	Cooling water	kg/kg-isopentenol	214.65	55.12	595.35	60.77
	Steam 180°C	kg/kg-isopentenol	0.57	0.22	1.10	0.12
	Electricity	kWh/kg-isopentenol	5.90	1.56	18.45	1.85
	Corn liquor	kg/kg-isopentenol	0.12	0.04	0.21	0.03
	Diammonium phosphate	kg/kg-isopentenol	0.01	0.01	0.03	0.00
	Enzyme	kg/kg-isopentenol	0.07	0.01	0.10	0.01
	Water	kg/kg-isopentenol	13.03	5.05	24.43	2.83
Recovery and separation	Air	kg/kg-isopentenol	218.79	49.17	670.15	86.66
	Cooling water	kg/kg-isopentenol	1373.65	541.14	2473.26	285.99
	Steam 226°C	kg/kg-isopentenol	26.96	10.29	49.37	5.74
	Steam 180°C	kg/kg-isopentenol	0.93	0.64	1.29	0.10
Wastewater treatment	Electricity	kWh/kg-isopentenol	0.08	0.03	0.15	0.02
	Steam 180°C	kg/kg-isopentenol	0.26	0.07	0.43	0.05
	Electricity	kWh/kg-isopentenol	0.32	0.12	0.60	0.07
	Water	kg/kg-isopentenol	18.82	6.82	33.38	3.97
	Air	kg/kg-isopentenol	26.90	9.75	47.71	5.67
Onsite energy generation	WWT nutrients	kg/kg-isopentenol	0.01	0.00	0.01	0.00
	Cooling water	kg/kg-isopentenol	665.42	239.33	1112.43	135.25
	Electricity	kWh/kg-isopentenol	0.36	0.13	0.60	0.07
	Natural gas	kg/kg-isopentenol	1.86	0.68	3.30	0.39
	Water	kg/kg-isopentenol	73.54	27.31	133.69	15.87
	Air	kg/kg-isopentenol	329.27	119.32	584.08	69.44

Note: μ : baseline (average) value; a: minimum value; b: maximum value; and σ : standard deviation.

'WWT' refers to wastewater treatment

S2. Capital and operating costs for isopentenol production system

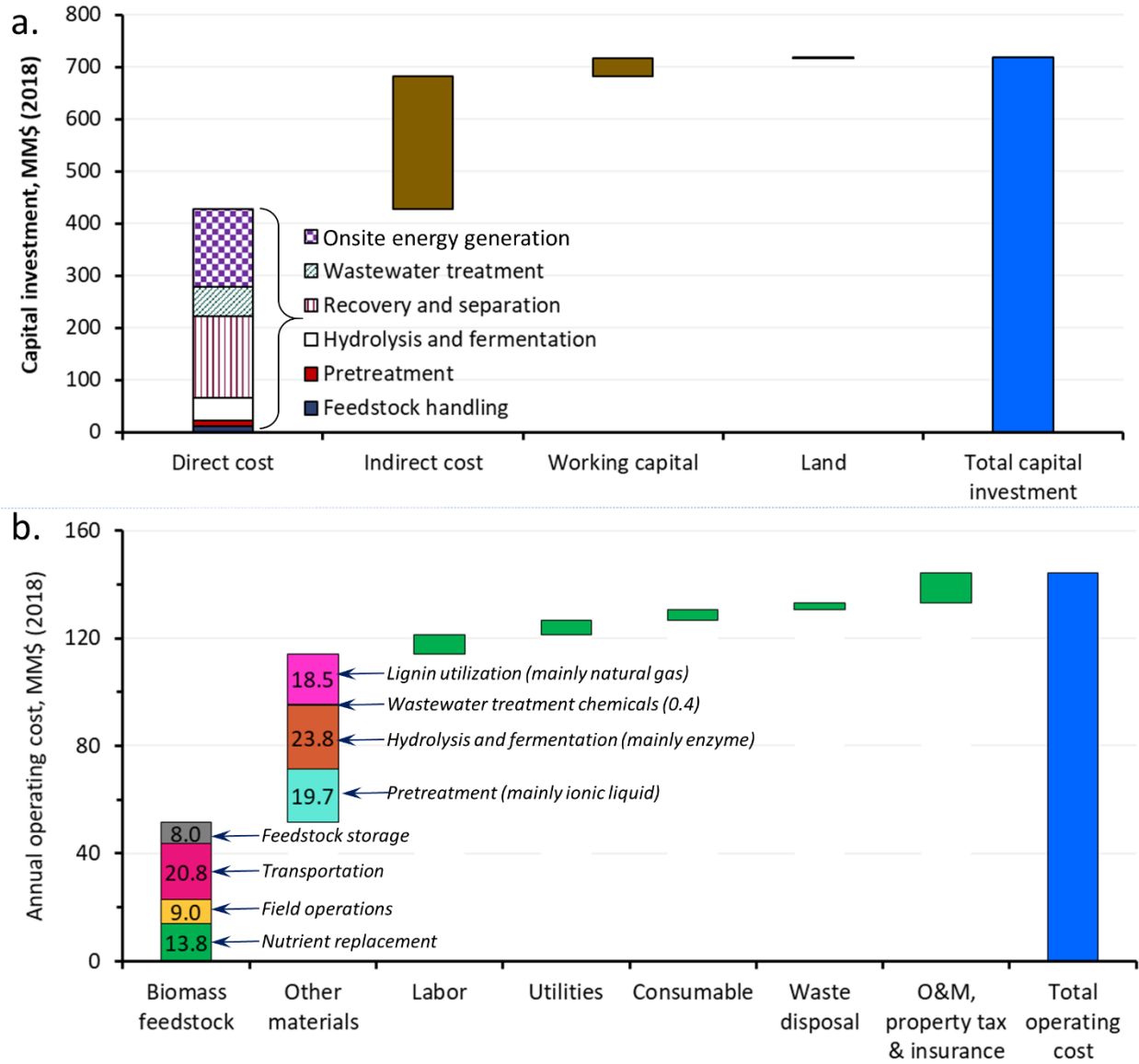


Figure S1. Capital investment (a) and annual operating cost (b) for isopentenol production system. The biorefinery utilizes 2000 dry metric ton of biomass sorghum per day and operates 330 days per year and 24 hours per day.

S3. Contributions of capital and operating costs to isopentenol selling price

Figure S2 indicates the contributions of major capital and operating expenses to overall minimum selling price of isopentenol in the baseline scenario (assuming 50% of theoretical yield). The detailed capital and operating costs are provided in the Figure S1. The total capital investment equates to \$10/L of production capacity (\$37.8/gal), which is 5.3 times greater than the dilute-acid-based cellulosic ethanol production facility studied by NREL,³⁵ due to both the difference in bioconversion route/yield and pretreatment process. Recovery and separation of the IL and isopentenol (including capital-intensive pervaporation⁵²), along with the combined heat and power (boiler and steam turbine³⁵) section, are the major contributors to direct fixed capital cost. Improved, lower-cost pervaporation systems or alternative IL recovery strategies could reduce the direct capital cost associated with recovery and separation. The direct fixed capital cost accounts for 59.4% of the total fixed capital. Indirect costs (engineering, construction, and overheads) account for 35.6% of the total capital investment (Figures S1 and S2).

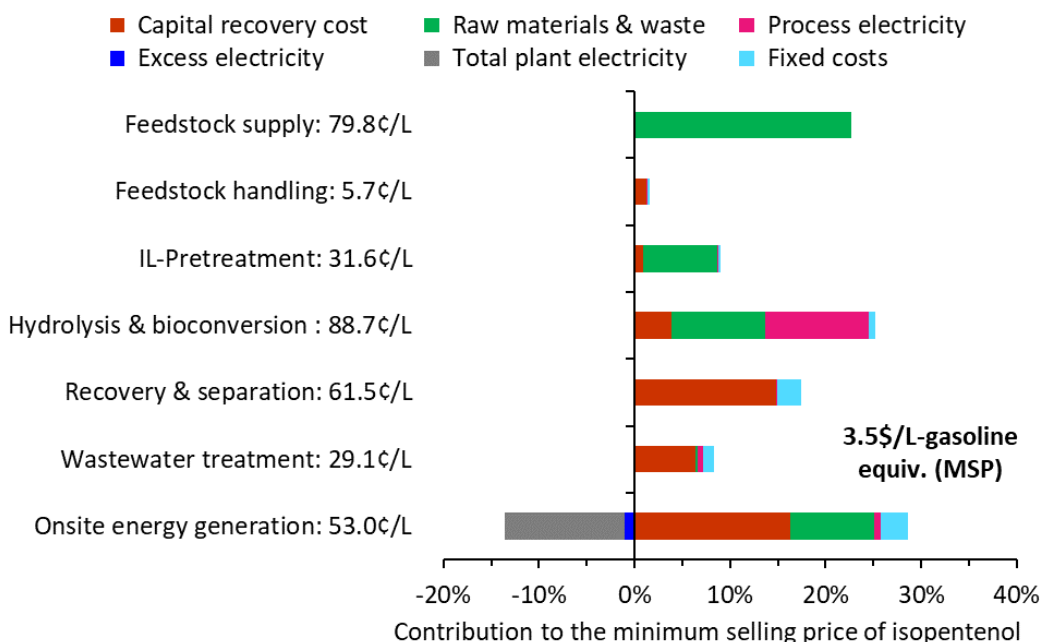


Figure S2. Baseline scenario costs for each stage of isopentenol production system, including capital and operating costs normalized on a per-liter basis.

Biomass feedstock supply is the single largest contributor to operating cost (35.7%), and other material inputs comprise another 43.3% (Figure S1). The major contributors to the feedstock supply cost are transportation and on-field nutrient inputs (Figure S1). Similarly, enzymes, the IL, and natural gas are major contributors to annual operating cost (Figures S1 and S2). Increasing the IL recovery rate and decreasing the enzyme loading can reduce the required makeup IL and enzymes, respectively, thus lowering operating costs. Additionally, switching from aerobic to a micro-aerobic process can eliminate the natural gas input (because lignin and biogas are sufficient fuel sources to provide the required electricity and process steam in the microaerobic case). Others, including labor, utilities, consumables, and overheads, account for about 20% of the total operating cost (Figures S1 and S2).

S4. Single point sensitivity analysis

S4.1. Minimum selling price

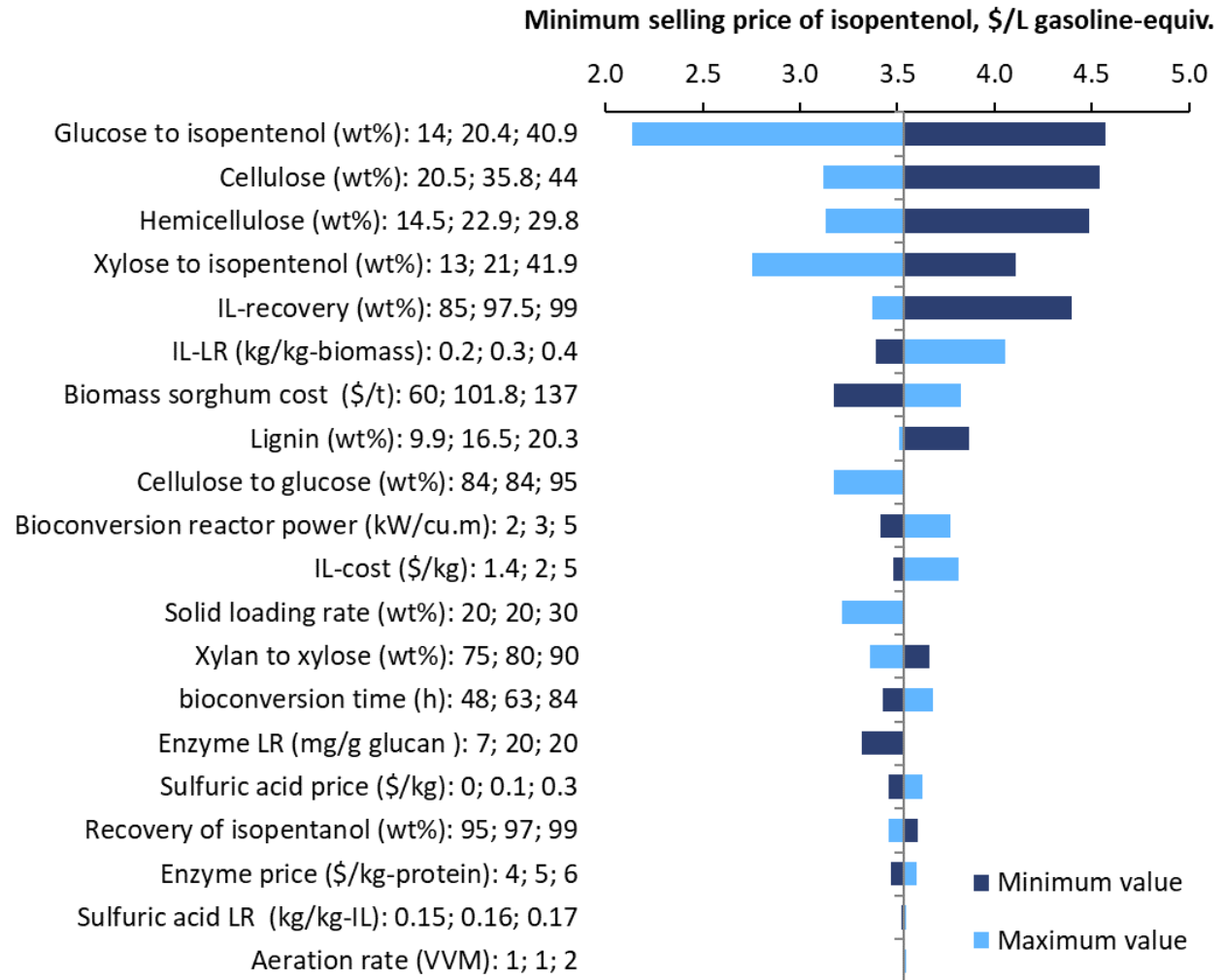


Figure S3. Most influential input parameters to the selling price of isopentenol

S4.2. GHG emissions

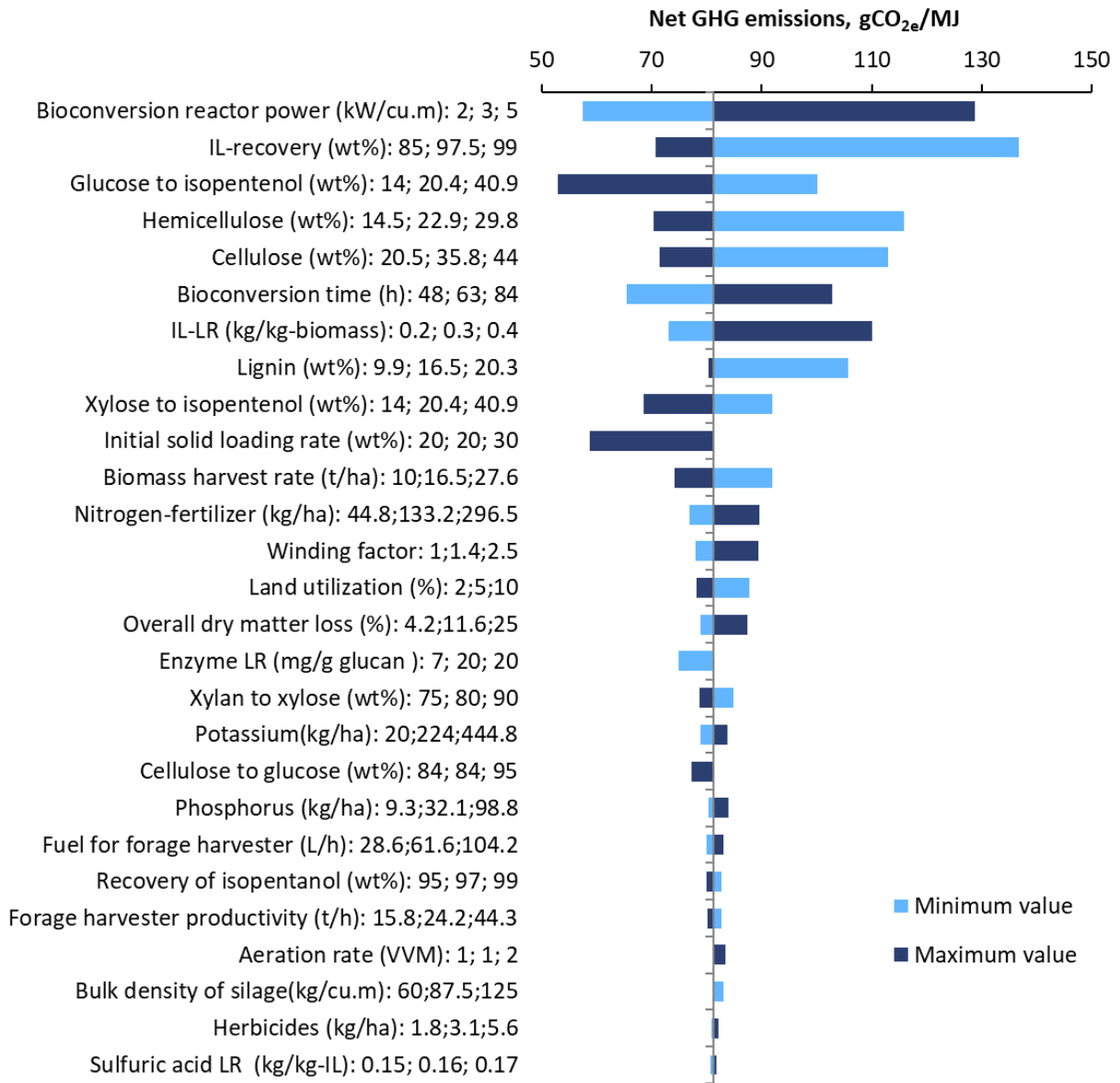


Figure S4. Most influential input parameters to GHG emissions associated with renewable isopentenol production

S4.3. Water consumption

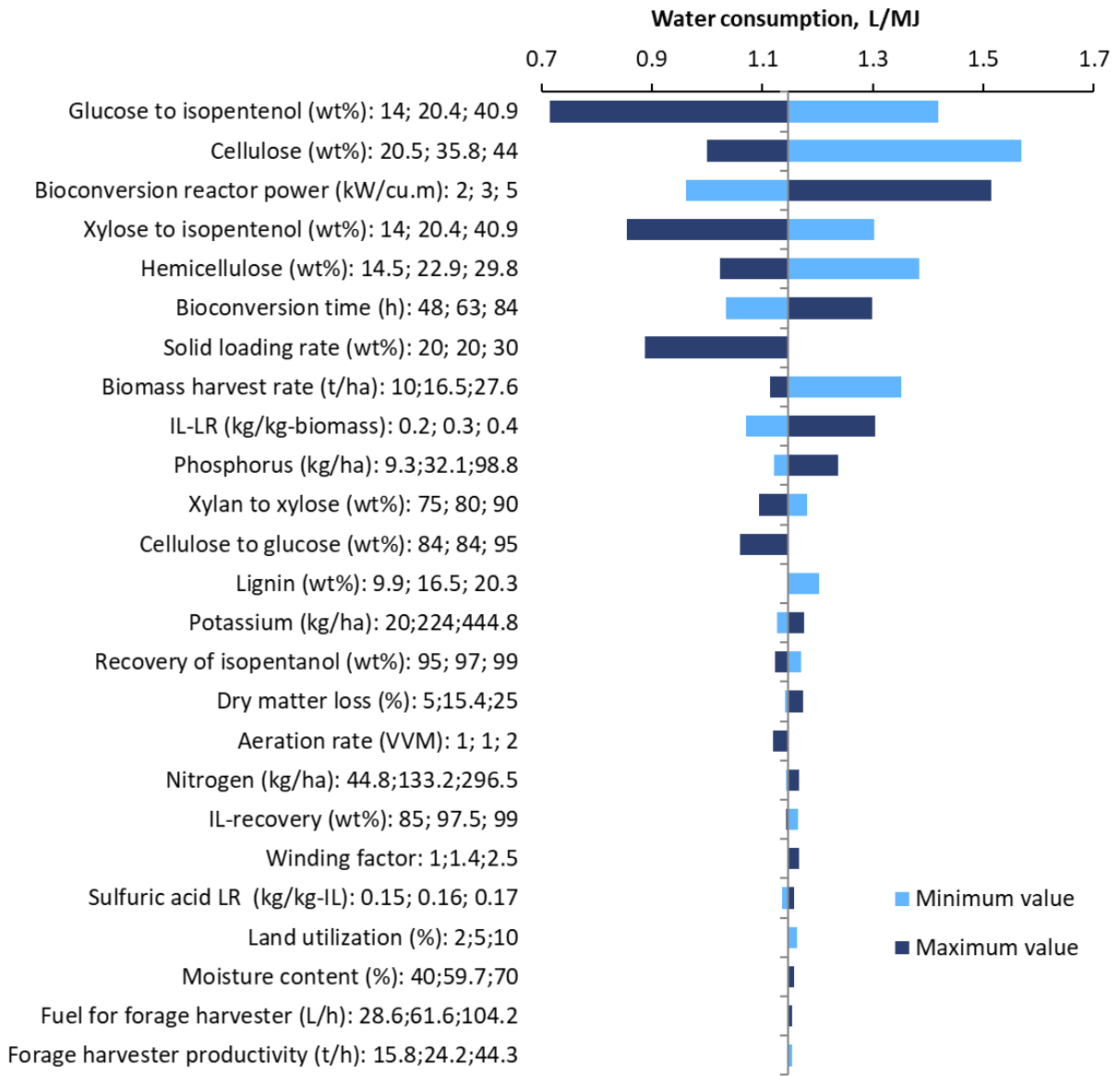


Figure S5. Most influential input parameters to water consumption for isopentanol production chain

S4.4. Water withdrawal

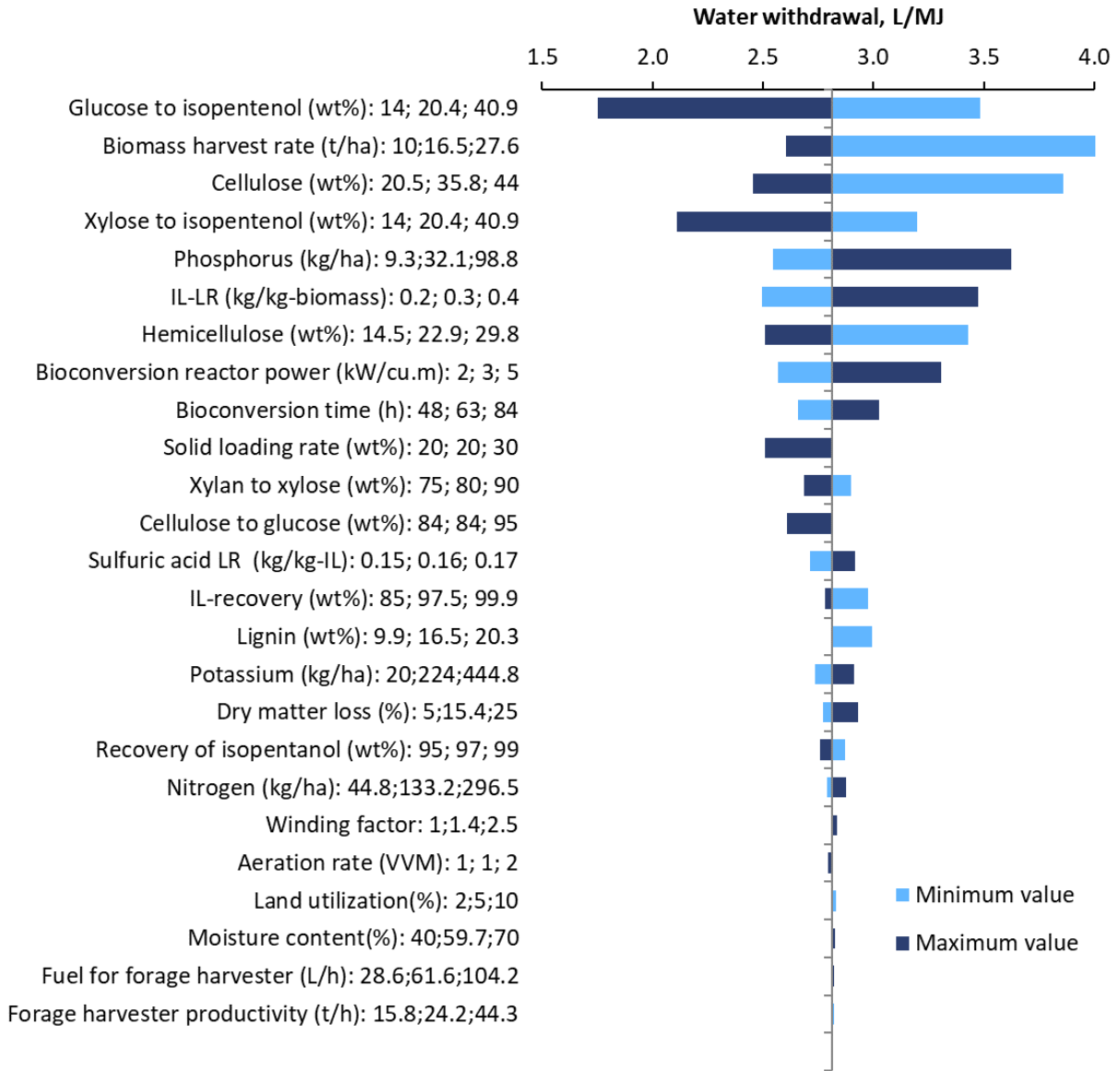
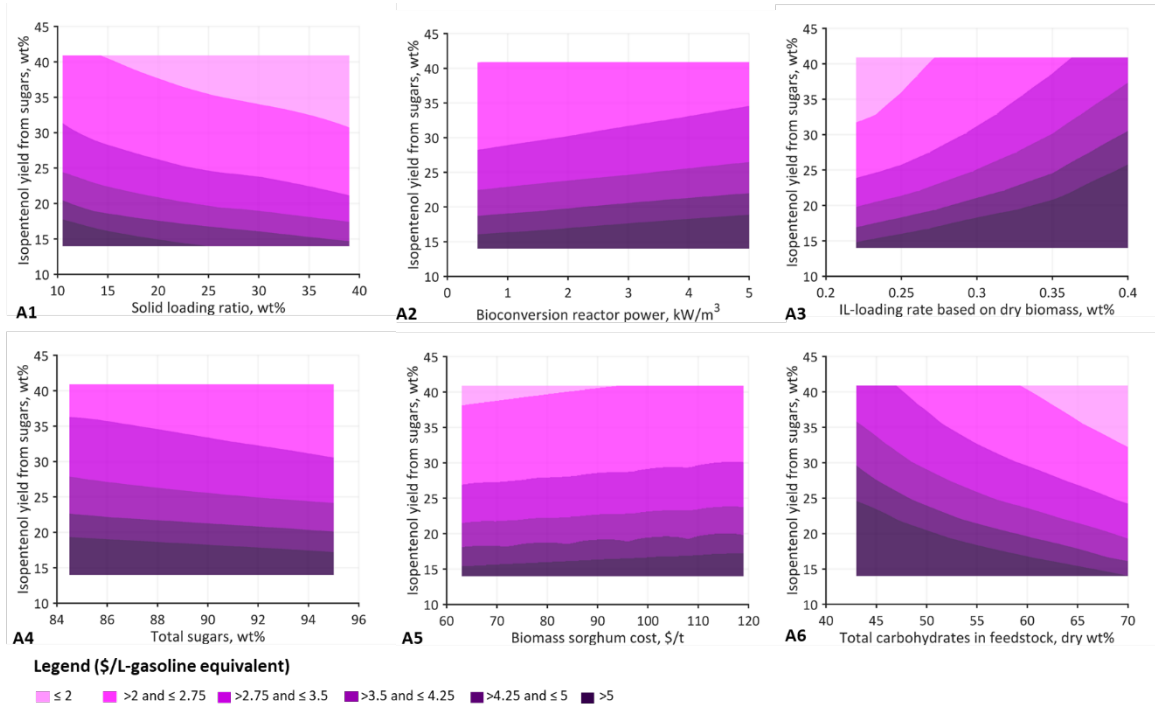


Figure S6. Most influential input parameters to water withdrawal for isopentanol production chain

S5. Selected most influential parameters to minimum selling price and GHG emissions: two-point sensitivity analysis

a. Minimum selling price



b. GHG emissions

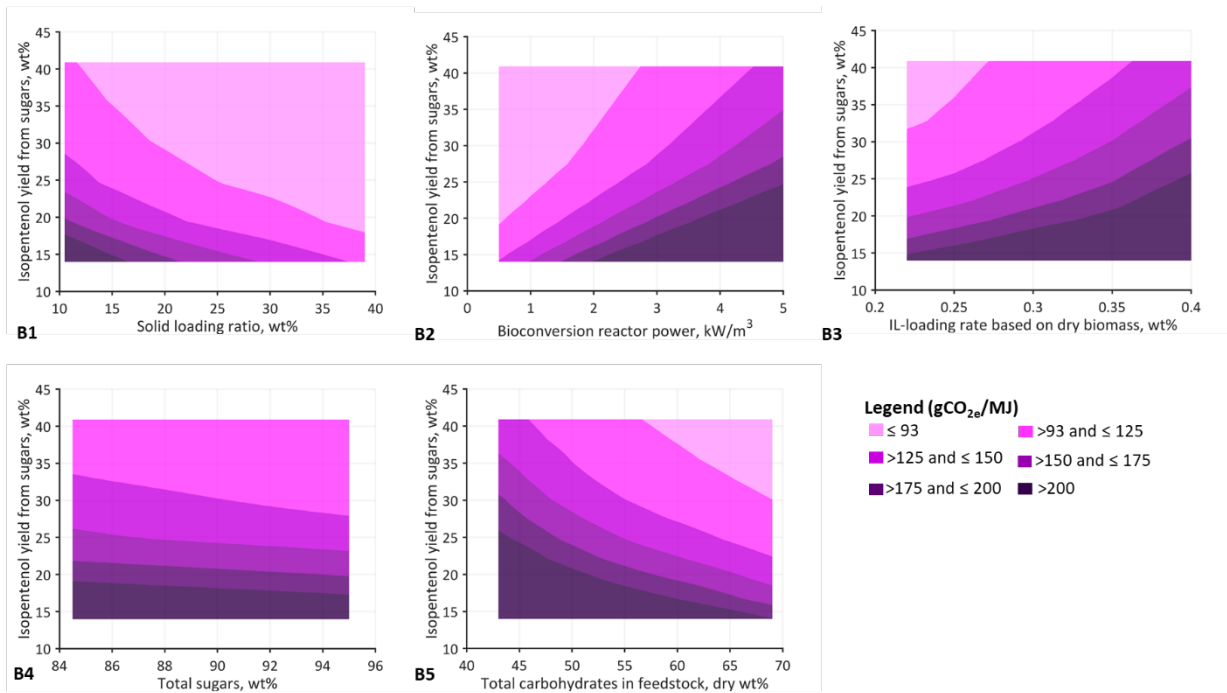
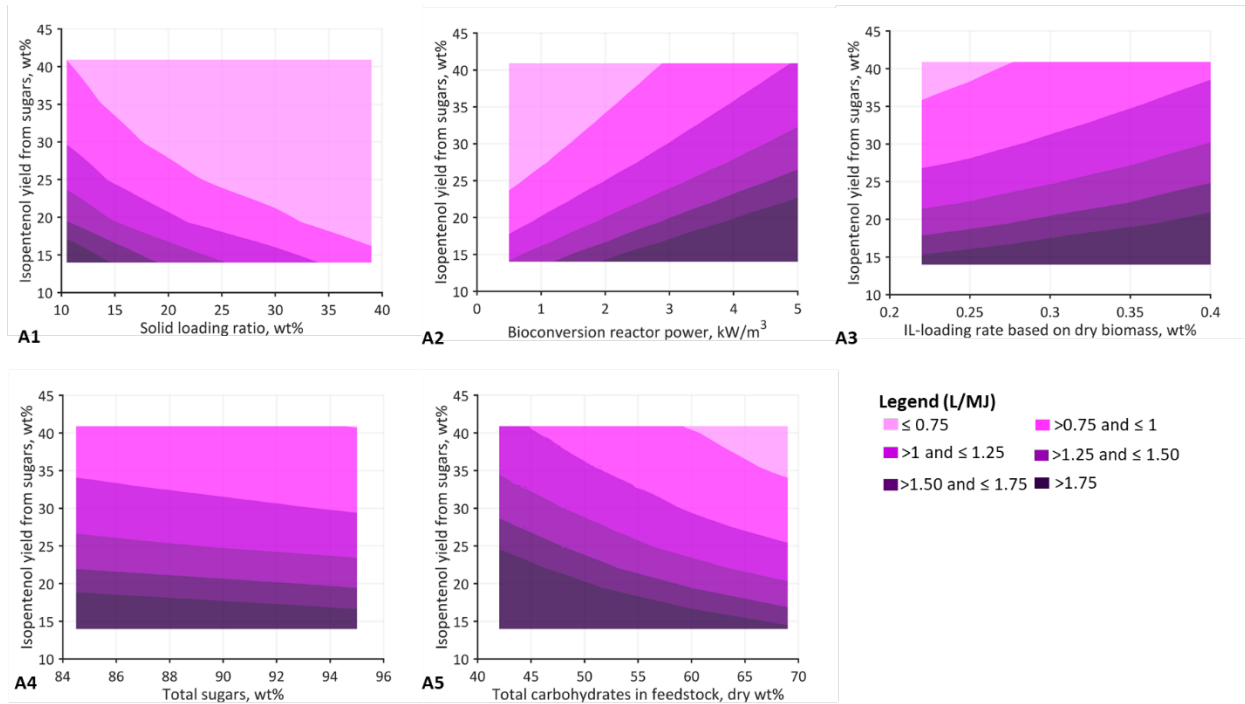


Figure S7. Heat maps with the selected influential parameters to the minimum selling price (A1 through A6) and GHG emissions (B1 through B5).

S6. Selected most influential parameters to water footprints

a. Water consumption



b. Water withdrawal

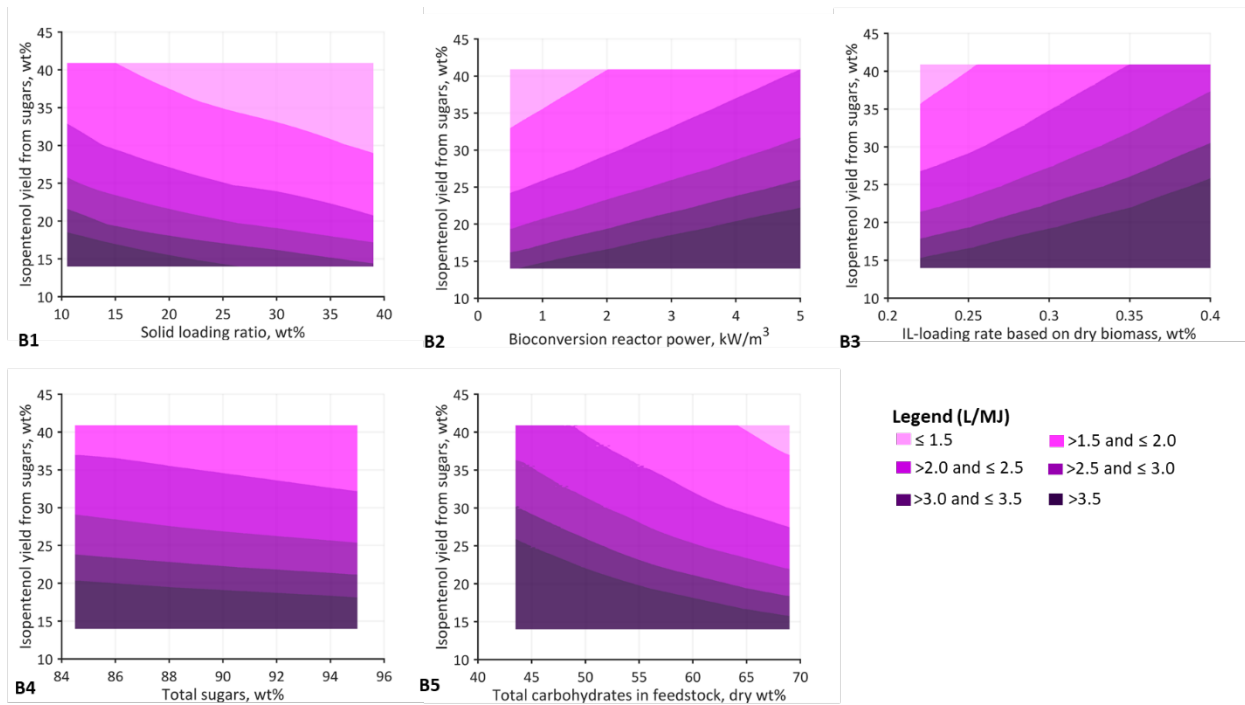


Figure S8. Heat maps with the selected influential parameters to water consumption (A₁ through A₅) and water withdrawal (B₁ through B₅).

S7. Probability distributions of the minimum selling price, GHG emissions, water consumption and water withdrawals for each life-cycle stage of the entire isopentenol production chain

S7.1 Uncertainty associated with minimum selling price

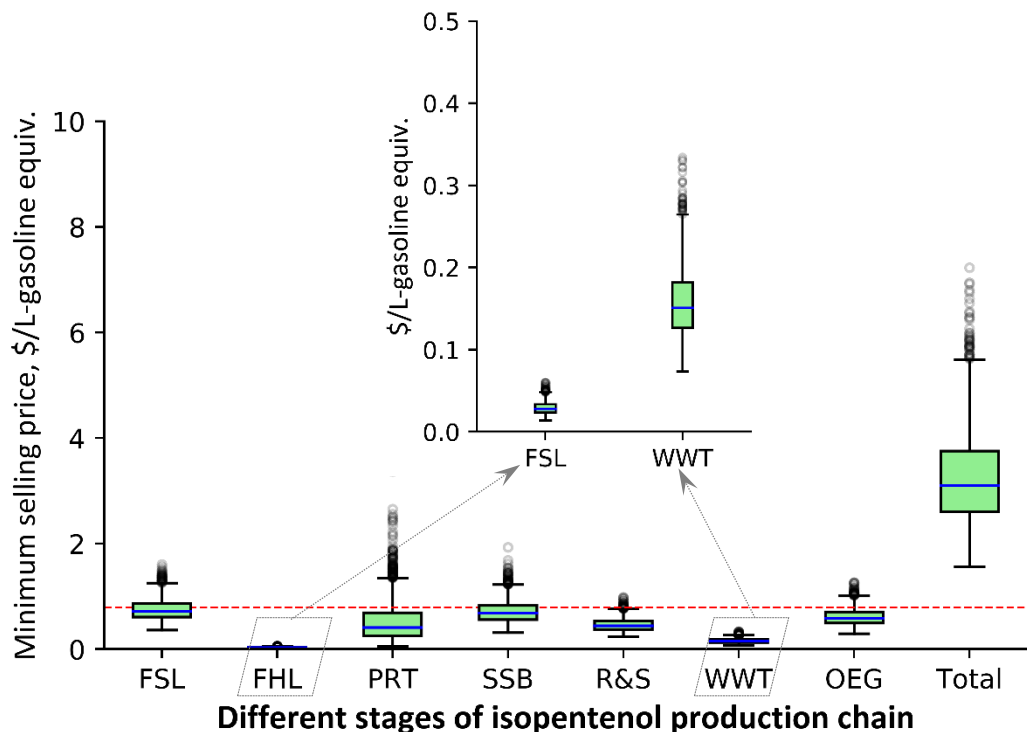


Figure S9. Uncertainty associated with the minimum selling price of isopentenol. In this figure, **FSL**: Feedstock supply logistics; **FHL**: Feedstock handling; **PRT**: Pretreatment; **SSB**: Simultaneous saccharification and bioconversion; **R&S**: Recovery and separation; **WWT**: Wastewater treatment; **OEG**: Onsite energy generation. The horizontal dashed line (- - -) refers to the targeted selling price of \$0.79/L-gasoline equivalent (\$3/gge).

S7.2 Uncertainty associated with GHG emissions

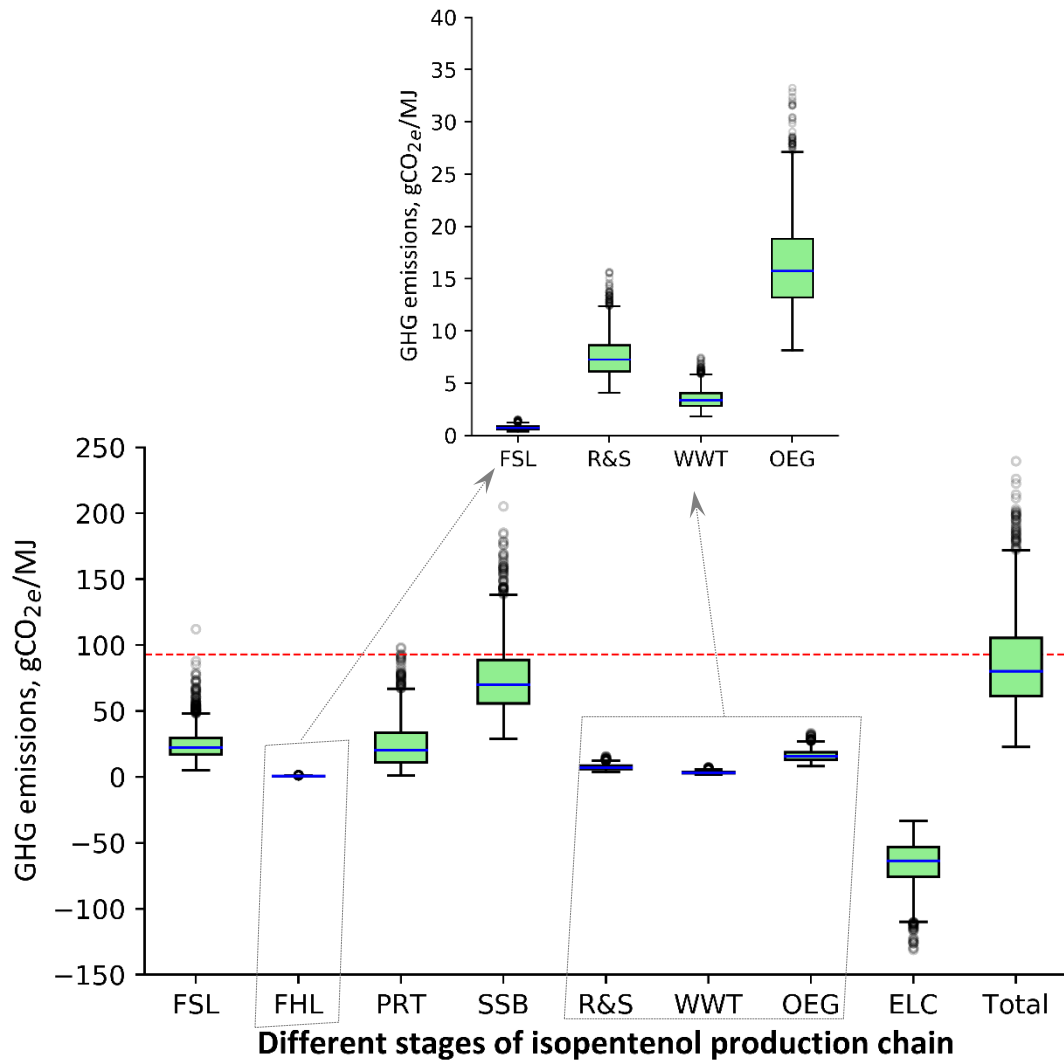


Figure S10. Uncertainty associated with GHG emissions. In this figure, **FSL**: Feedstock supply logistics; **FHL**: Feedstock handling; **PRT**: Pretreatment; **SSB**: Simultaneous saccharification and bioconversion; **R&S**: Recovery and separation; **WWT**: Wastewater treatment; **OEG**: Onsite energy generation; **ELC**: onsite electricity credits; and **Total**: Net GHG emissions. The horizontal dashed line (- - -) refers to the GHG emissions from gasoline of 93 gCO_{2e}/MJ.

S7.3 Uncertainty associated with water consumption

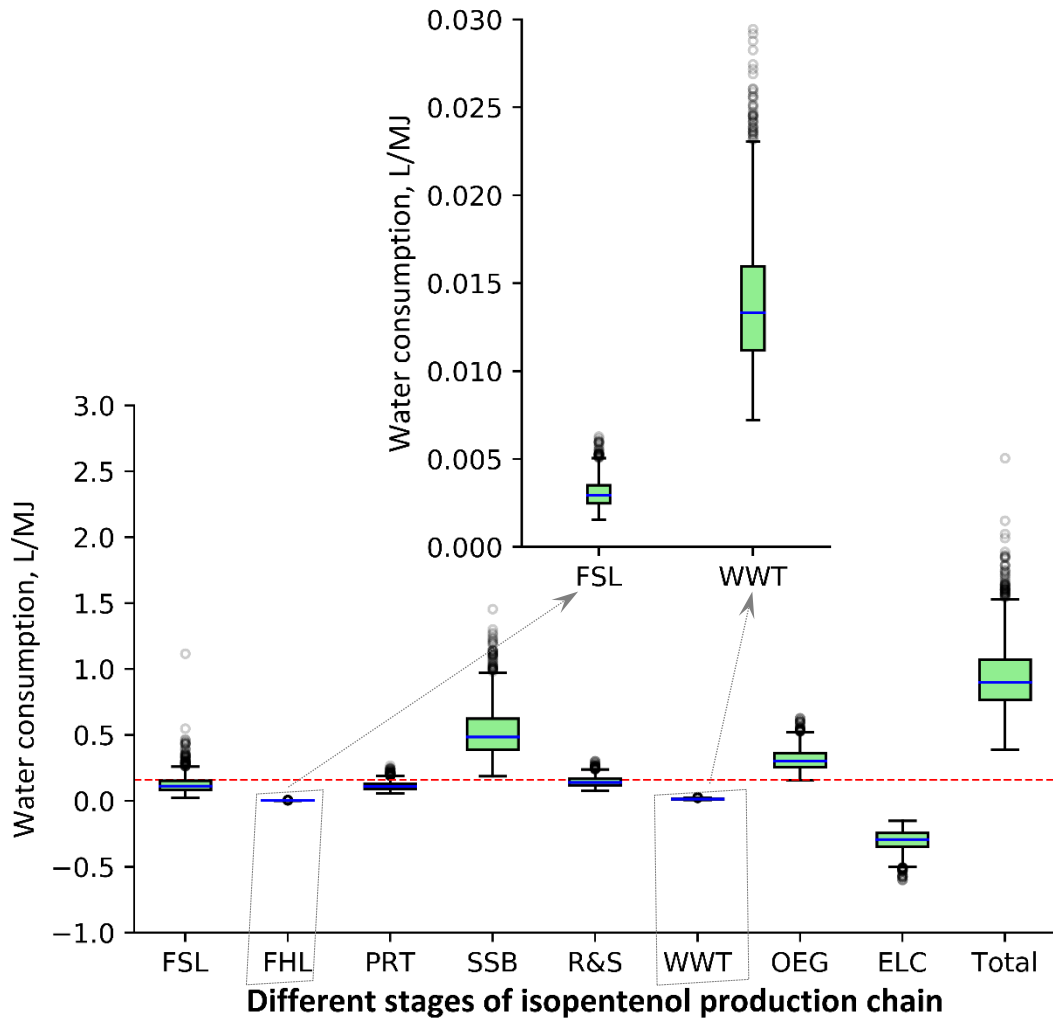


Figure S11. Uncertainty associated with water consumption. In this figure, **FSL**: Feedstock supply logistics; **FHL**: Feedstock handling; **PRT**: Pretreatment; **SSB**: Simultaneous saccharification and bioconversion; **R&S**: Recovery and separation; **WWT**: Wastewater treatment; **OEG**: Onsite energy generation; **Direct**: Direct water consumption at biorefinery; **ELC**: onsite electricity credits; and **Total**: Net water consumption. The horizontal dashed line (---) refers to water consumption for gasoline of 0.16 L/MJ.

S7.3 Uncertainty associated with water withdrawals

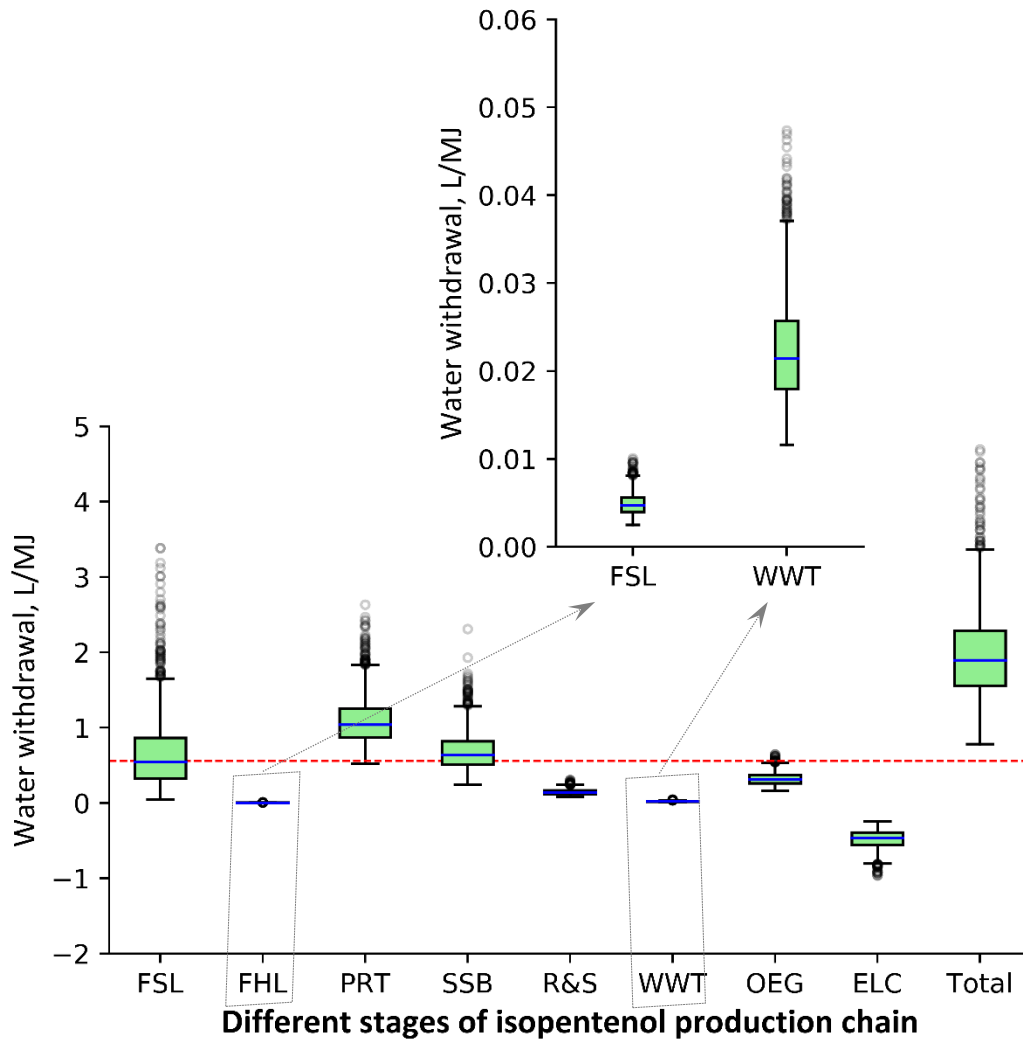


Figure S12. Uncertainty associated with water withdrawals. In this figure, **FSL**: Feedstock supply logistics; **FHL**: Feedstock handling; **PRT**: Pretreatment; **SSB**: Simultaneous saccharification and bioconversion; **R&S**: Recovery and separation; **WWT**: Wastewater treatment; **OEG**: Onsite energy generation; **ELC**: onsite electricity credits; and **Total**: Net water withdrawal. The horizontal dashed line (- - -) refers to water withdrawal for gasoline of 0.56 L/MJ.

S8. Optimal process conditions and isopentenol selling price

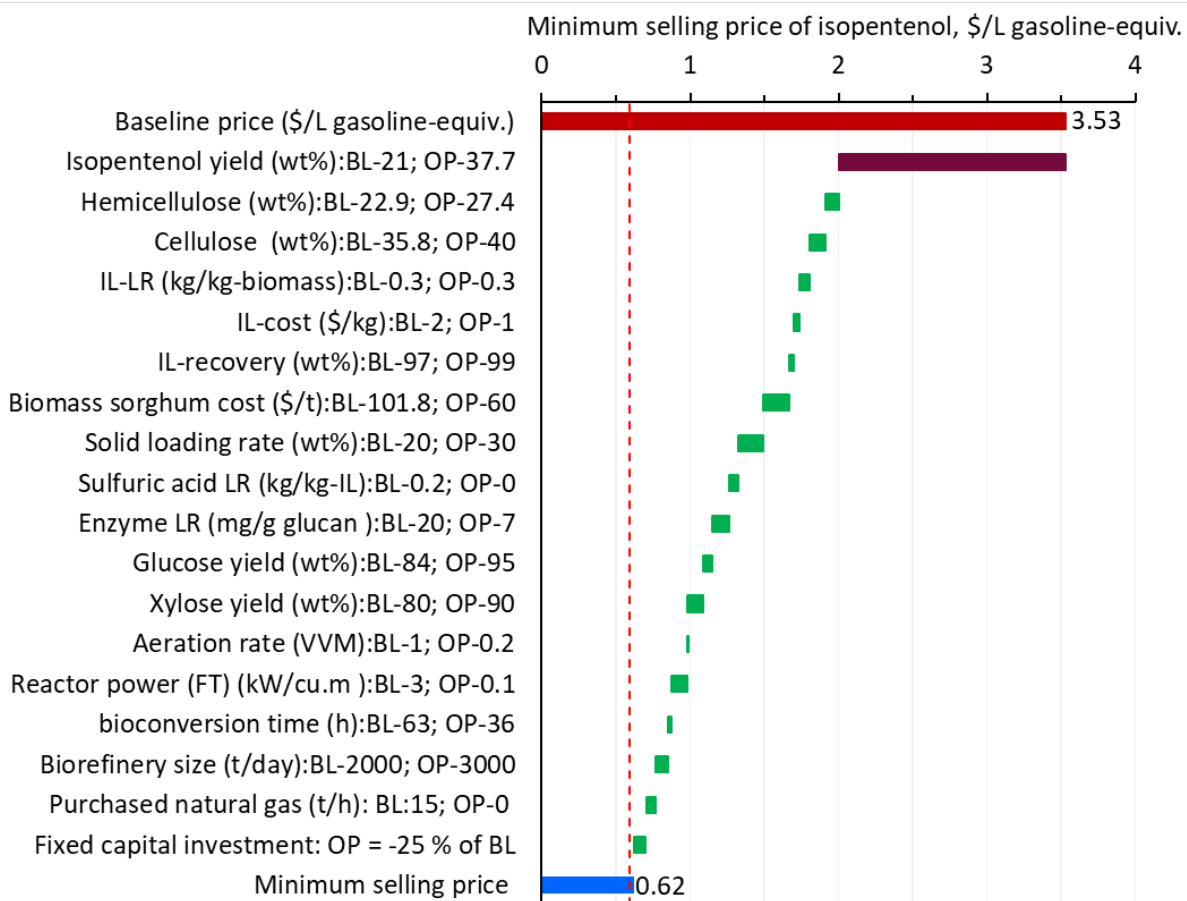


Figure S13. Pathways to achieve optimal selling price of isopentenol. In this figure 'BL' refers to the baseline and 'OP' refers to the optimal.

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